

**SIM PROJECT
PRELIMINARY INSTRUMENT SYSTEM
REQUIREMENTS REVIEW
(PISRR)**

***SIM Dynamics & Control Requirements
Flowdown Process
17-18 March, 1998***

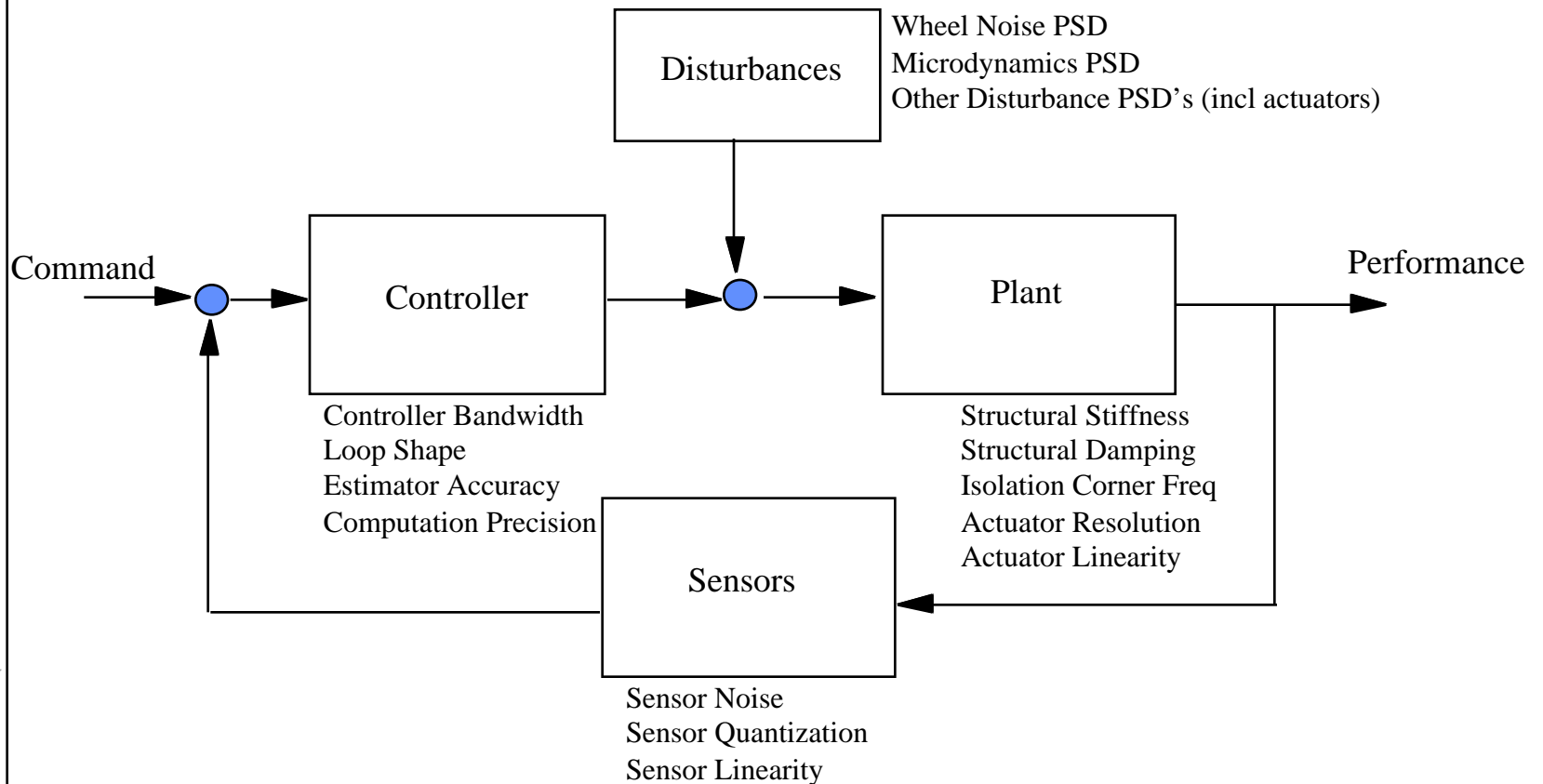
***Robert A. Laskin
STB-3 Architect***

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 - Role of integrated modeling & testbeds
- Summary/Conclusion

Motivation

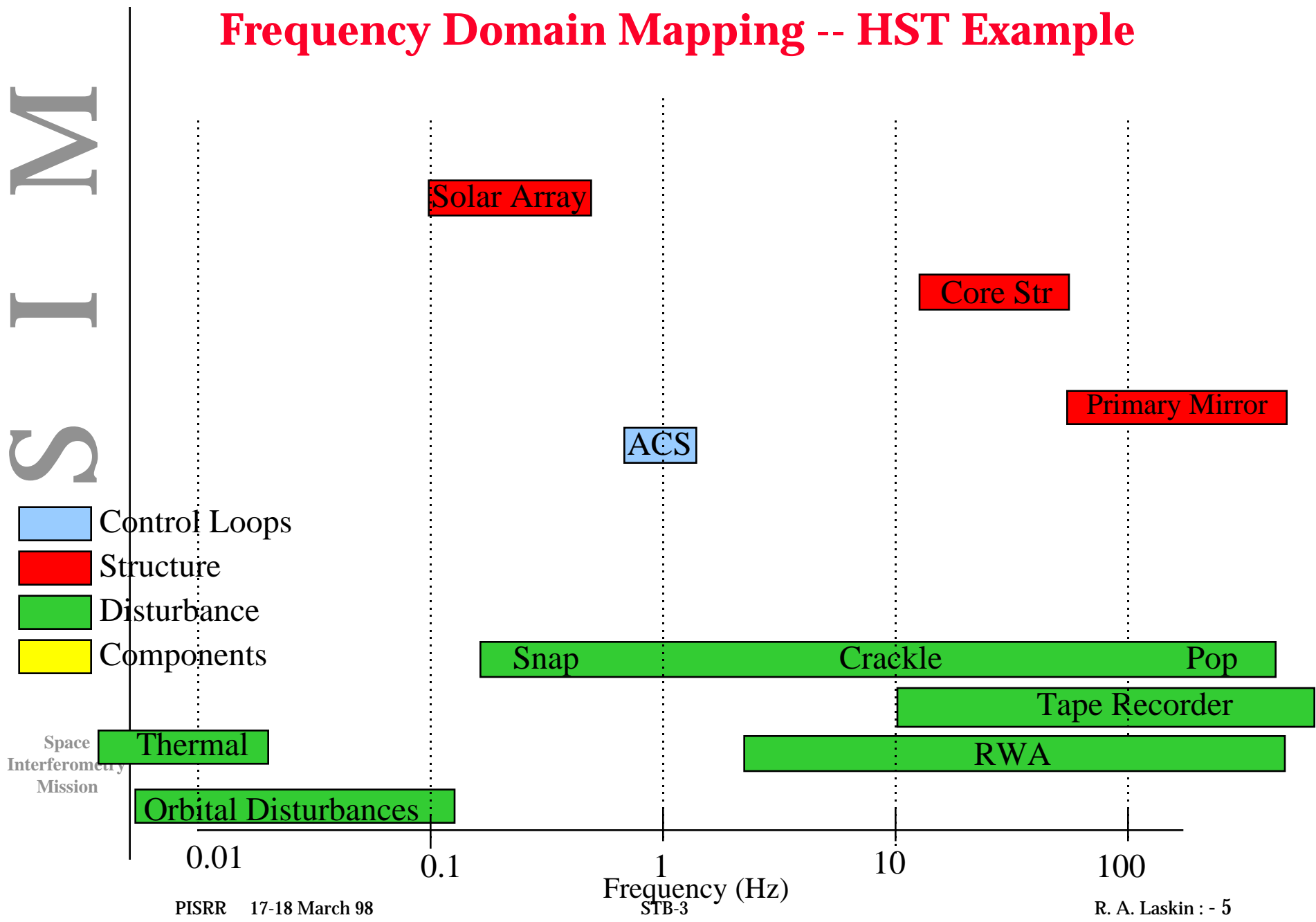
- Dynamics & control requirements tend to crosscut multiple subsystems
=> trades need to be made at the system level



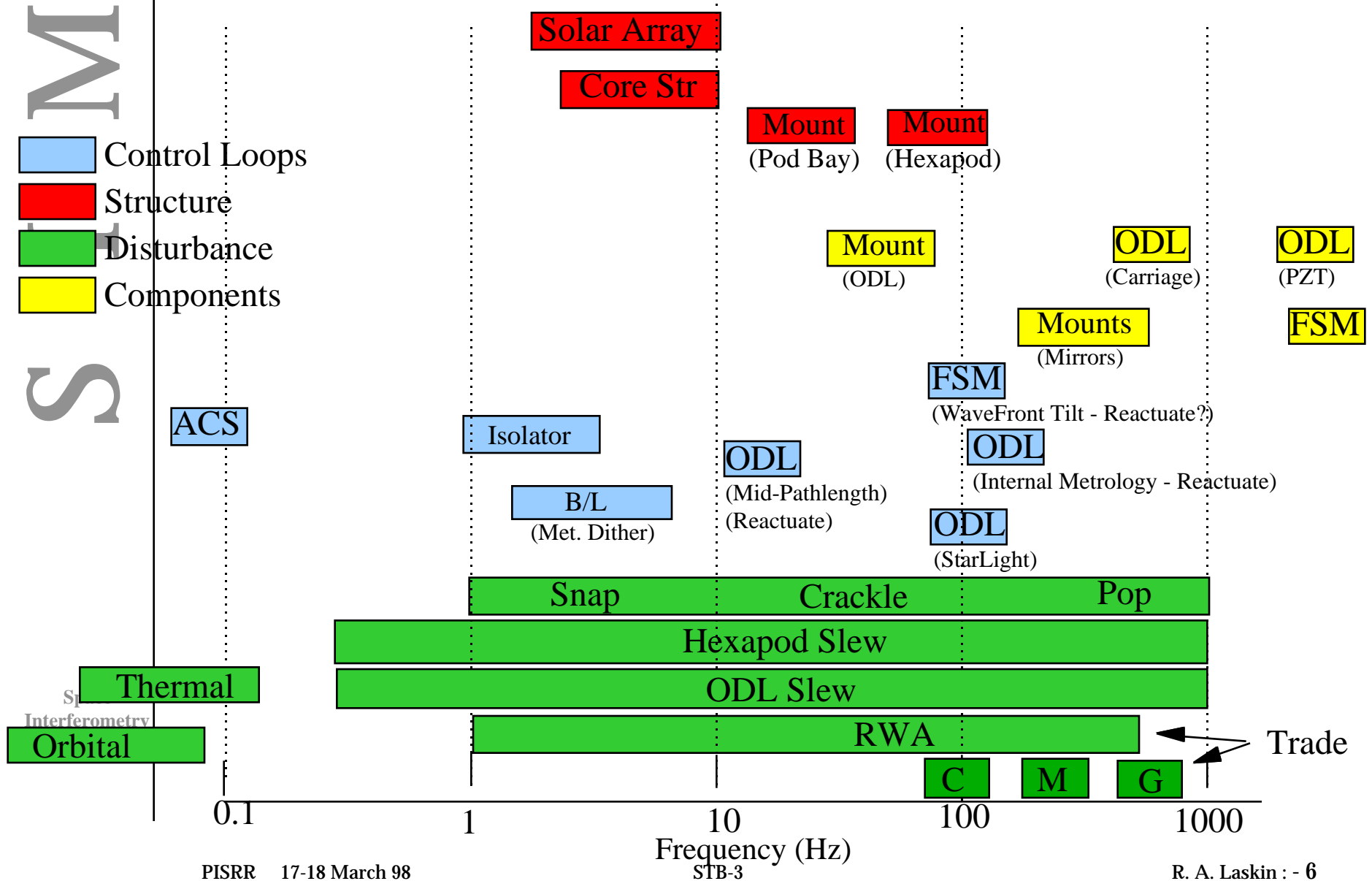
Frequency Domain Mapping

- Determine the critical temporal frequencies that govern major parts of the system
 - Disturbance frequencies
 - > space environment -- thermal radiation, solar pressure
 - > on-board machinery
 - > microdynamics -- snap, crackle, pop
 - Control system bandwidths
 - > ACS
 - > active optics
 - Structural modes
 - > appendage modes
 - > core structure modes
 - > optical bench mounting modes
 - > optical component mounting modes
- Try to enforce frequency separation if possible
- Bootstrap: disturbance freq => control BW => structural freq
- Can trade amplitude for frequency separation

Frequency Domain Mapping -- HST Example



Preliminary SIM Frequency Domain Mapping



Rule of Thumb Based Requirements Allocation

- ACS bandwidth < 0.1 Hz
 - disturbances are all low frequency
 - amplitudes are low
 - pointing requirement is modest
- Core structure fundamental frequency > 5 Hz (stiff as practical)
 - wide separation from ACS bandwidth
 - minimize thermal deformation
 - hold tight alignment tolerances
 - minimize vibration transmission
- Actuated body much stiffer than control loop
 - FSM 1000 Hz
 - ODL PZT mounted mirror 3 kHz
- Reactuate where structural interaction with support structure is likely
 - ODL PZT
 - ODL Voice Coil
 - FSM?

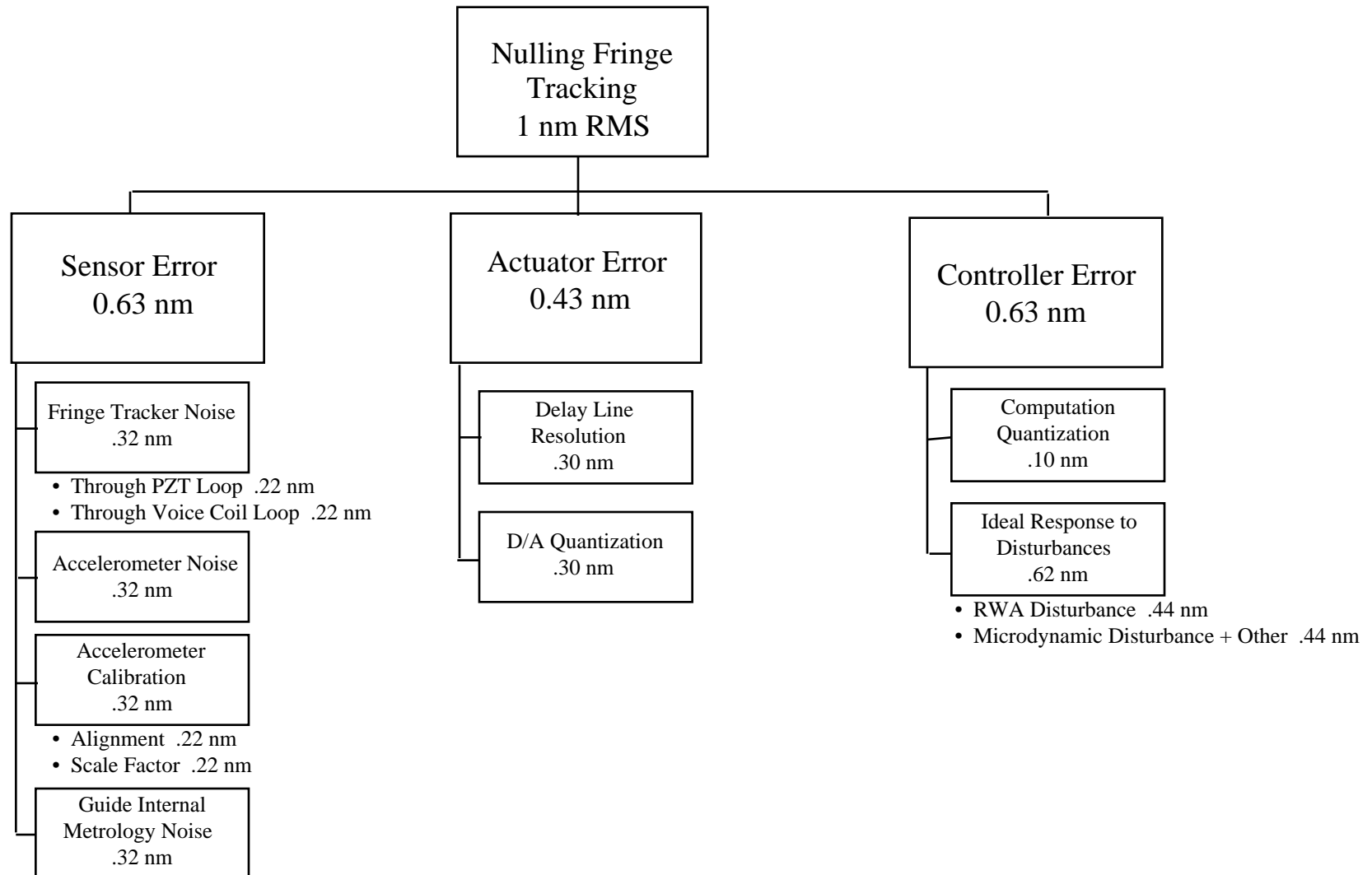
Error Budget Based Requirements Allocation

- Develop a dynamics & control error budget for each system mode
- Allocate errors to an a priori “level of equal pain” using engineering judgement
 - what is equal pain (cost, schedule, technical risk)
 - will top level requirement be met
- Reallocate errors in an iterative fashion
 - based upon models & analysis
 - > integrated models: controls, structure, optics
 - > start simple: optical sensitivity matrix, modal gain analysis, shock spectrum analysis, preliminary disturbance models, controller “filters”
 - > increase fidelity over time (e.g., incl. pod, hex, optics modes)
 - > put the requirements into the model
 - based upon testbed and bench testing
 - > STB-1 and STB-3
 - > component testing
 - based upon screams of pain (calibrate the whiners)

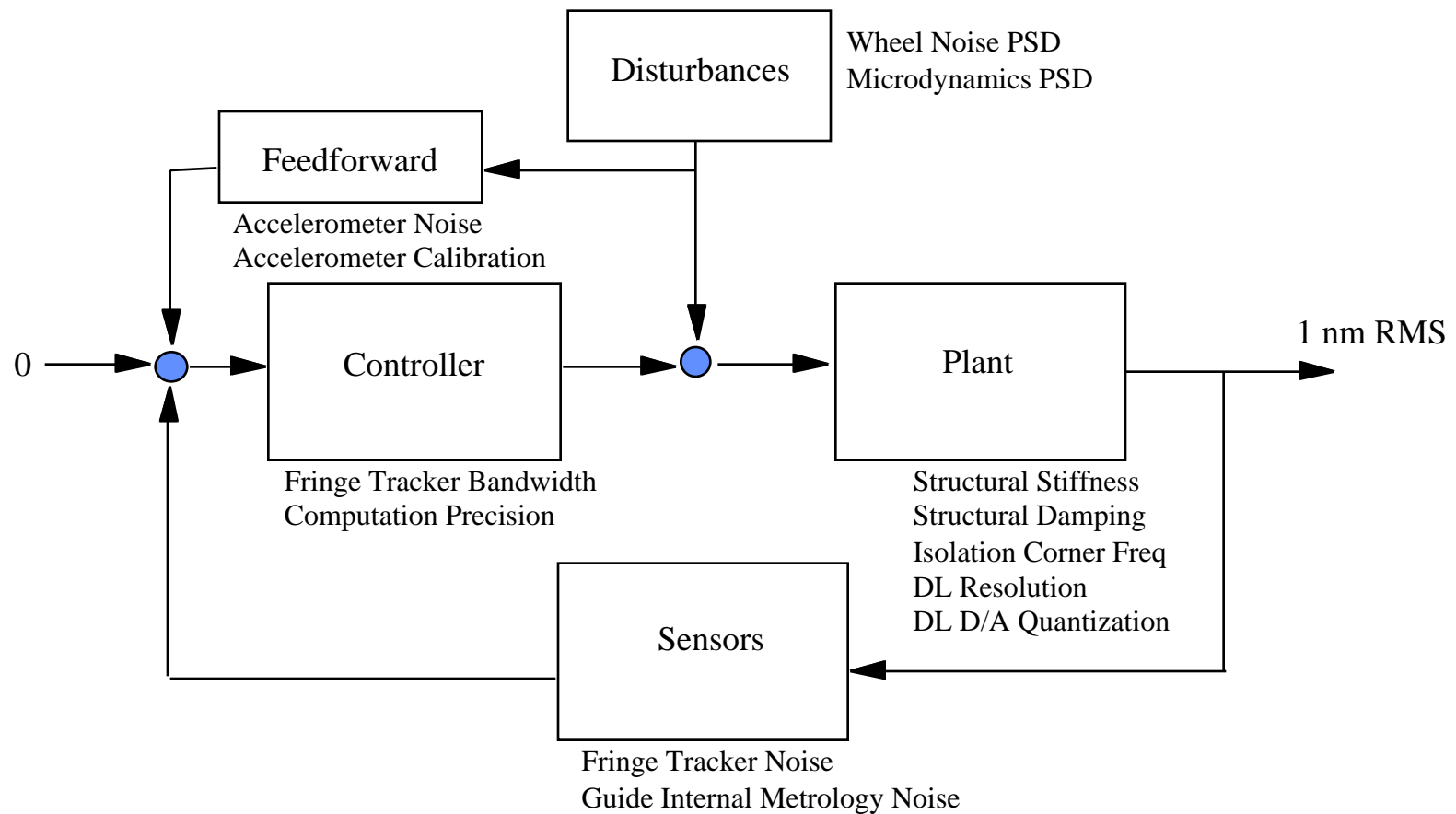
SIM Dynamics & Control Error Budgets

- Nulling Fringe Tracking - 1nm
- Nulling Angle Tracking - TBD mas (TBD mas on sky)
- Guide Star Fringe Tracking - 10 nm
- Science Star Fringe Tracking - 10 nm
- Guide Star Angle Tracking - 30 mas (30 mas on sky, 330 mas on detector)
- Science Star Angle Tracking - 30 mas
- Guide Star Fringe Acquisition - 80 nm
- Science Star Fringe Placement (for Acquisition) - 25 um
- Guide Star Angle Placement (for Acquisition) - 1 arcsec
- Science Star Angle Placement (for Acquisition) - 3 arcsec
- Fringe and Angle Tracking for Imaging - TBD nm, TBD mas
- Guide Fringe Lock During Slews - TBD nm jitter
- Guide Angle Lock During Slews - TBD mas jitter
- Metrology Lock During Slews - TBD nm jitter
- Settling Time Post Slews - TBD seconds

Example -- 1 nm Pathlength Stabilization

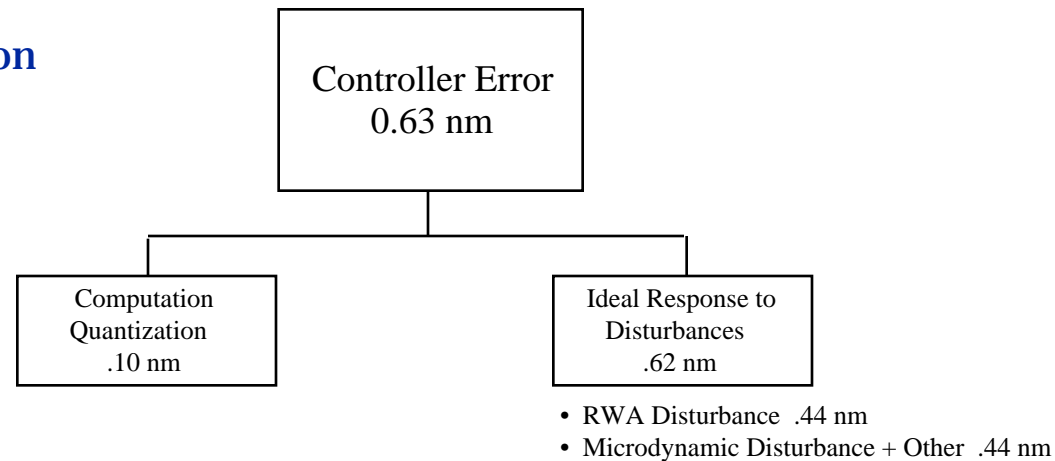


Example -- 1 nm Pathlength Stabilization



Controller Errors

- Error Allocation



- Derived Requirements

Computational Precision shall be less than .05 nm

Reaction Wheel Emitted Vibration (measured blocked) shall be less than Jim Melody Model

Isolator Corner Frequency shall be less than 2 Hz

Hardback 1st Modal Frequency shall be greater than 5 Hz

Hardback Modal Damping Ratio shall be greater than .1%

Collector Pod 1st Modal Frequency shall be greater than 25 Hz

Collector Pod Modal Damping Ratio shall be greater than .1%

Fringe Tracking Closed Loop BW (incl accels) shall be greater than 100 Hz

Persistent Microdynamics Background Vibration (typical point on structure) shall be less than 10 ug/rt(N)*

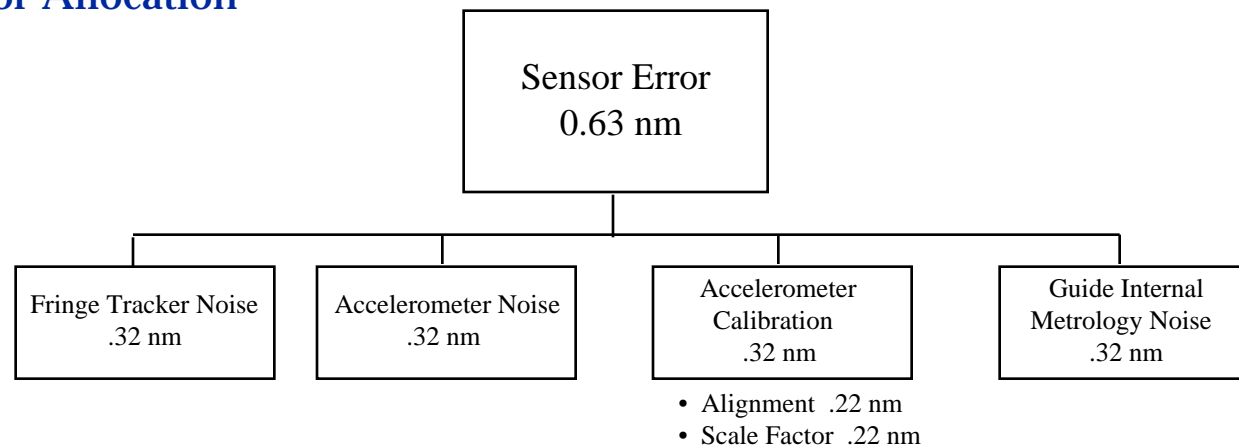
Transient Microdynamics Disturbance Response (typical point on structure) shall be less than 1 cm/s or 50 nm

Transient Microdynamics Disturbance Response (typical point on structure) shall occur less than once per 10 minutes

* N = number of bounces in interferometer beam train

Sensor Errors

• Error Allocation

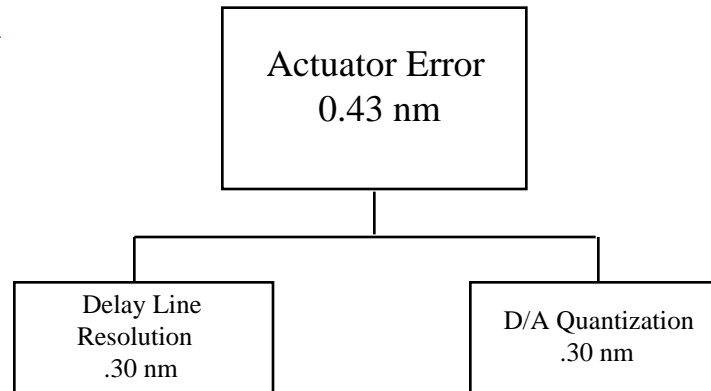


• Derived Requirements

- Fringe Tracker Noise within PZT Loop BW shall be less than .09 nm
- Fringe Tracker Noise beyond PZT Loop BW shall be less than .09 nm (post-filtering)
- Fringe Tracker Noise within VC Loop BW shall be less than .09 nm
- Fringe Tracker Noise beyond VC Loop BW shall be less than .09 nm (post-filtering)
- Accelerometer Noise within PZT Loop BW shall be less than .09 nm
- Accelerometer Noise beyond PZT Loop BW shall be less than .09 nm (post-filtering)
- Accelerometer Noise within VC Loop BW shall be less than .09 nm
- Accelerometer Noise beyond VC Loop BW shall be less than .09 nm (post-filtering)
- Accelerometer Calibrated Alignment to sensed axes shall be less than 260 urad (1 um amp, sin)
- Accelerometer Scale Factor Calibration shall be less than .026% (1 um amplitude motion)
- Internal Metrology Sensor Noise shall be less than TBD

Actuator Errors

- Error Allocation



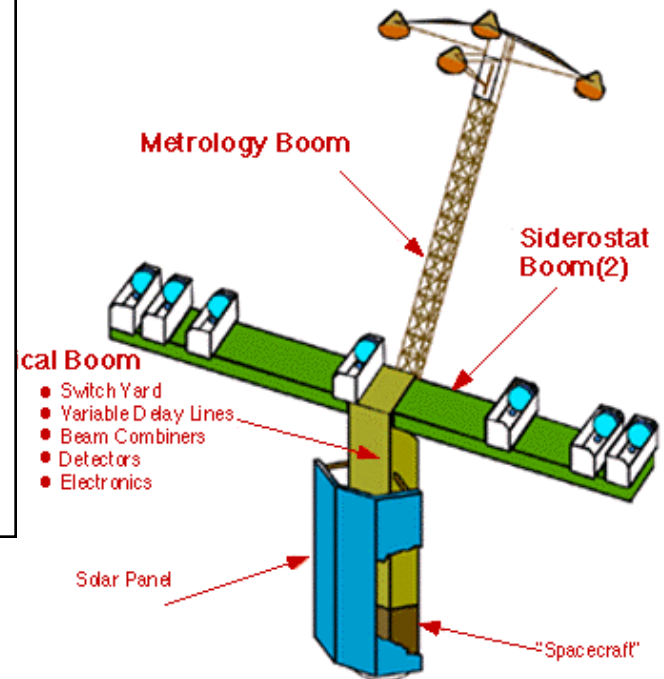
- Derived Requirements

PZT Mechanical Resolution shall be less than .15 nm

A/D Quantization Cmd to PZT shall be less than .15 nm

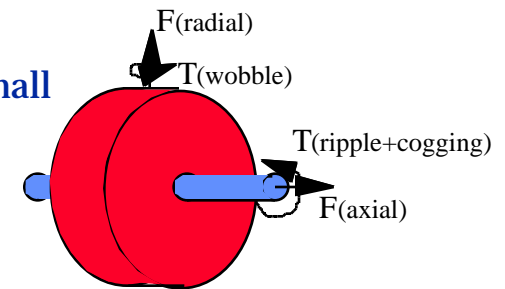
SIM Classic 3 Baseline Integrated Model

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isoview_3bsim6.eps
Creator:
MATLAB, The Mathworks, Inc.
Preview:
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with a preview included in it.
Comment:
This EPS picture will print to a
PostScript printer, but not to
other types of printers.



Disturbance Analysis

- Hubble Space Telescope Harmonic Disturbance RWA Model
 - Model Force/Torque Induced Vibration as Blocked Force
 - Assume Spin Motor Disturbance (Ripple and Cogging) Small
 - Stochastic Broadband Model
 - Discrete-Frequency RWA Model
 - > Sweep over wheel speeds (0 to 3000 RPM)
- OPD vs. RPM
 - Each Point Represents Standard Deviation of the Discrete Frequency PSD of OPD Resulting From the Disturbance of a Single RWA at a Given Speed

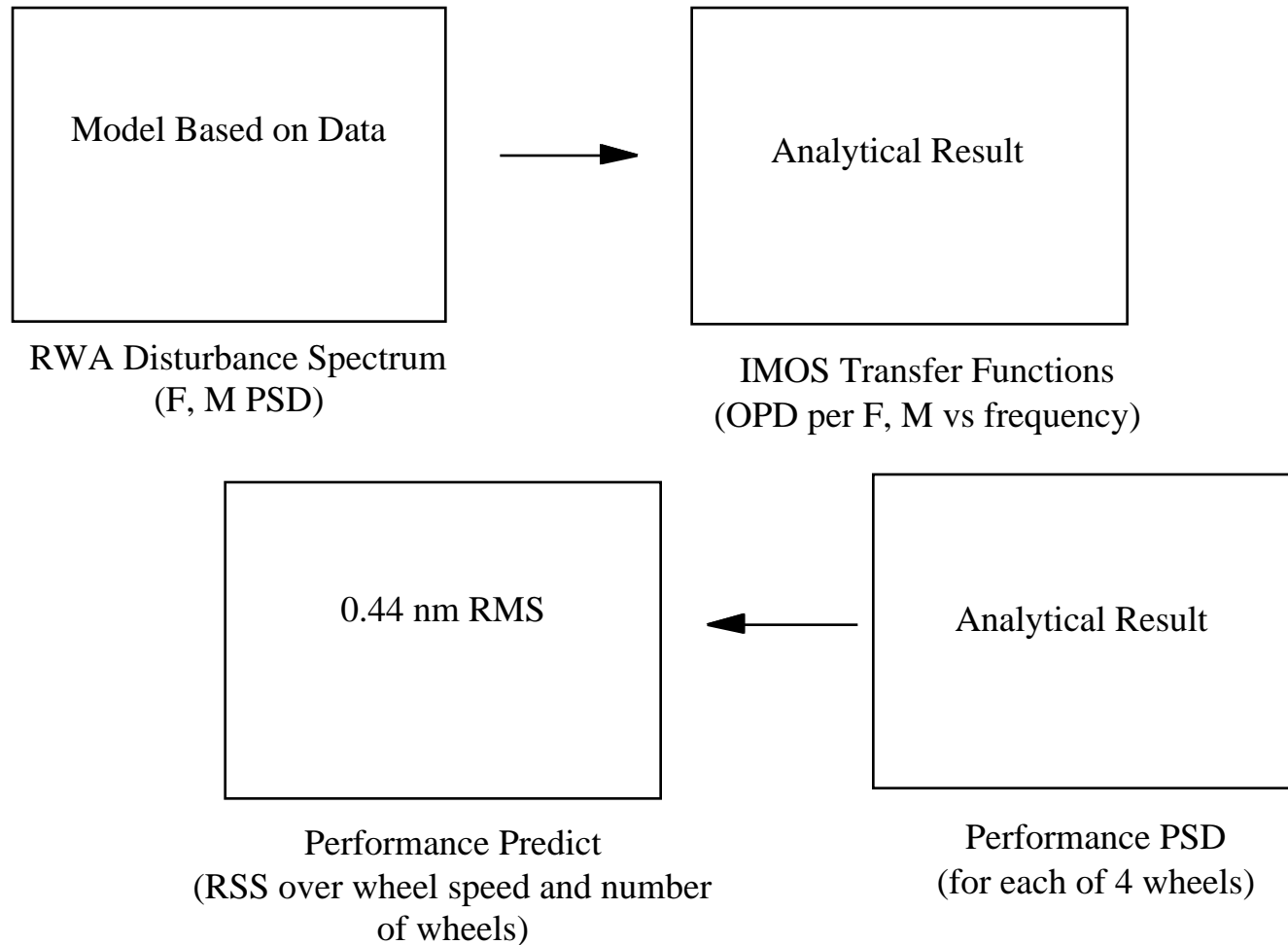


$$IV(t) = \sum_{i=1}^n C_i f_{RWA}^2 \sin(2 h_i f_{RWA} t + \phi_i)$$

$$S_{opd}^2(f_{RWA}) = \left| G(j\omega) \frac{OPD}{RWA} \right|^2 (f_{RWA}) d$$

- RWA High Frequency Signature Is Unique
 - Bearing Geometry, Bearing Race, Cage Speed, Operating Temp, Lubrication, Life
 - Model Flexibility Rolloffs With Parameterized Filters
 - Housing Flexibility, Bearing Impedance (100 Hz)
 - Statistically Bound Problem Using Many RWA Models

Performance Prediction with IMOS Model



Sensitivity Chart

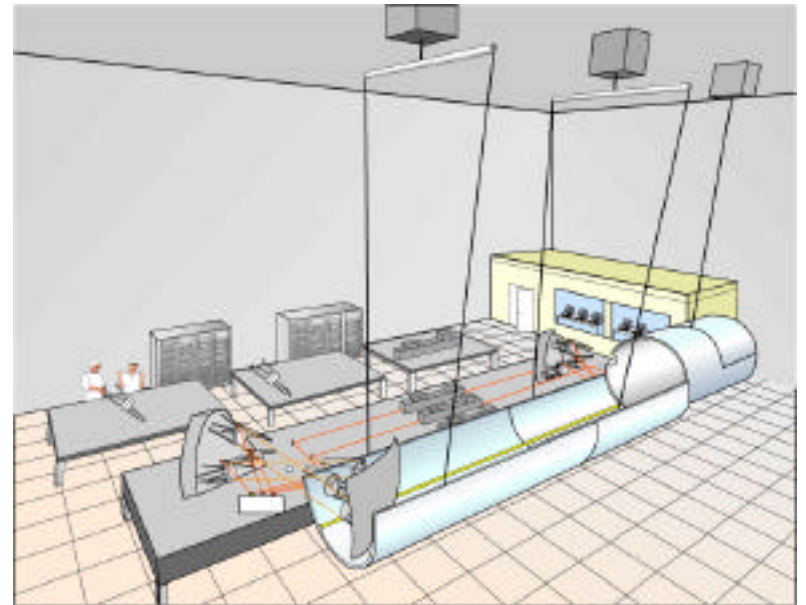
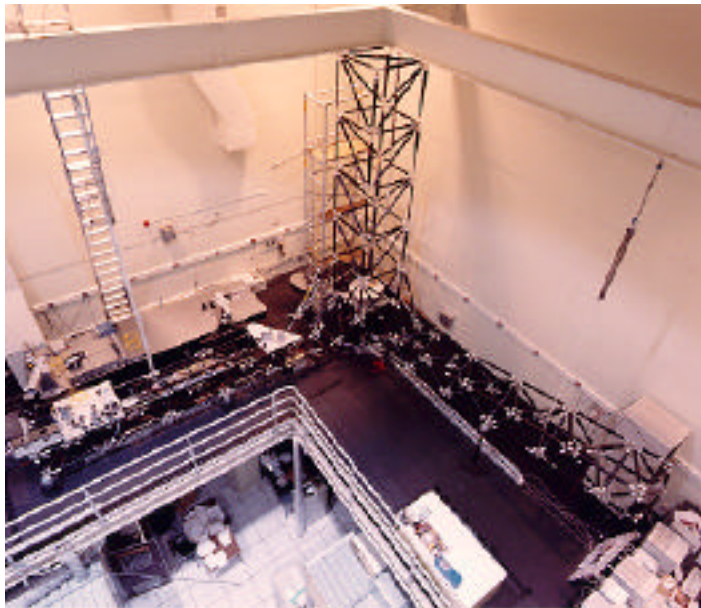
S
I
M

Space
Interferometry
Mission

Testbed Reality Chart

Hardware Testing Makes It Real

- The testbeds inform the process of dynamics/control requirements allocation in two major ways:
 - Supply real numbers to put in the error budget boxes
 - Validate the allocation process
 - > same methodology is applied to the testbeds
 - > error propagation assumptions can be checked
- STB-1 and STB-3 -- where the rubber meets the road for dynamics and control requirements flowdown



Summary

- Defined a process for flowdown of SIM dynamics/control requirements
- Need to work the process for the new architecture
=> Begin building a low complexity integrated model ASAP
- STB-1 and STB-3 will be key system testbeds for validating dynamics/control requirements flowdown/flowup